STUDY OF LIME VS. NO LIME IN COLD IN-PLACE RECYCLED ASPHALT CONCRETE PAVEMENTS

Final Report

by

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September 1991

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1. Report No.	2. Government Accession No.	3. Recipient's Catalog No.			
OR-RD-92-02					
4. Title and Subtitle		5. Report Date			
Study of Lime vs. No Lime in Co	ld In-place Recycled Asphalt	September 1991			
Concrete Pavements		6. Performing Organization Code			
7. Author(s)		Performing Organization Report No.			
Haiping Zhou and Scott Nodes	ñ				
9. Performing Organization Name and Add	lress	10. Work Unit No. (TRAIS)			
Oregon State Highway Division					
Materials and Research Section 800 Airport Road S.E.		11. Contract or Grant No.			
Salem, Oregon 97310					
12. Sponsoring Agency Name and Address	3	13. Type of Report and Period Covered			
Oregon State Highway Division		Final Report			
Materials and Research Section 800 Airport Road S.E. Salem, Oregon 97310		14. Sponsoring Agency Code			
15. Supplementary Notes					

16. Abstract

The resilient characteristics of cold in-place recycled asphalt concrete with and without lime were examined. Six core samples were obtained from a site two months after construction; six months later, six additional core samples were obtained from the site. The samples were tested in the laboratory for resilient modulus. Conclusions of this study include:

- 1. The resilient modulus of the recycled mix with lime increased substantially in the early stage, as compared to the recycled mix without lime.
- 2. The resilient modulus value of the recycled mix with lime after freeze-thaw conditioning was much higher than the recycled mix without lime.
- 3. Eight months after construction, the resilient modulus of the unconditioned recycled mix with lime was similar to that of the unconditioned recycled mix without lime.

Recommendations of this study include:

- 1. Further evaluate the potential benefit of adding lime to the recycled mix and investigate the effects of adding different percentages of lime to the recycled mix.
- 2. Evaluate the effects of adding quick lime compared to hydrated lime to the recycled mix.
- 3. Appropriate mix design criteria, construction procedures, and field control guidelines should be developed if adding lime to the recycled mix.

17. Key Words		18. Distribution Statement	
PAVEMENTASPHALT, RECYCLI MODULUS	NG, COLD, RESILIENT		
19. Security Classif. (of this report)	20. Security Classif. (of this page)	21. No. of Pages	22. Price
Unclassified	Unclassified		

ACKNOWLEDGEMENTS

The authors appreciate the cooperation of Tony George (Materials Unit, Oregon State Highway Division) and his staff for conducting the tests in the laboratory. In addition, the authors are grateful for Tony George, Dale Allen (Oregon State Highway Division), and Dave Rogge (Oregon State University) for their review of this report. Furthermore, the authors thank Stephanie Swetland and Jo Anne Robison for typing this report.

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STUDY OF LIME VS. NO LIME IN COLD IN-PLACE RECYCLED ASPHALT CONCRETE PAVEMENTS

1.0 INTRODUCTION

In the summer of 1990, a six-mile section of pavement on the Central Oregon Highway, as part of the Arnold Cave - Horse Ridge Section project, was recycled using the cold in-place process. The eastbound (EB) lane of this project had lime added to the recycled mix while the westbound (WB) lane was recycled without the use of lime.

To investigate the possible benefits of adding lime to the cold in-place recycled (CIR) mix, Region 4 and the Research Unit of the Oregon State Highway Division (OSHD) conducted a mini-study on the recycled mix with and without lime. The focus of this study was on the resilient characteristics of the recycled mix with and without lime.

This report documents the initial findings from the laboratory tests on limited core samples.

2.0 PROJECT DESCRIPTION

2.1 Pavement Condition

This section of pavement was constructed in the mid-1970's. The existing pavement condition (1990) was poor with an average of 3/4" rutting and severe fatigue cracking in all four wheelpaths (Appendix A).

2.2 Traffic Condition

This section of highway received an average daily traffic (ADT) of 1,000, of which 23% was truck traffic, based on the 1988 traffic data assembled by the Pavements Unit of the OSHD.

3.0 PROJECT EVALUATION

3.1 Core Samples

A total of twelve core samples were obtained and tested in the laboratory for resilient modulus. Six of the twelve cores were obtained approximately two months after construction while another six cores were obtained approximately eight months after construction. For each batch of six samples, three had lime and three had no lime.

3.2 <u>Lime Used</u>

Two percent of quick lime was added to the recycled mix.

3.3 Recycle Agent

For this study, pavement cores with a 0.4% CMS-2S recycle agent were evaluated.

3.4 Resilient Modulus Tests

The core samples were tested for resilient modulus in accordance with the ASTM D4123 procedure. For each sample, the resilient modulus before and after freeze-thaw conditioning was measured. Then, the Index of Retained Modulus (IRM) was calculated. Table 1 summarizes the test results on cores that were obtained two months after construction. Table 2 presents a summary of test results on cores that were obtained eight months after construction. The test results are also plotted in Figure 1. Detailed test results are included in Appendix B.

Table 1. Summary of Test Results on Cores Obtained Two Months after Construction

Sample			Resilient Me		
I.D.	Location	(Top, in)	Unconditioned	F-T Conditioned	IRM (%)
		a) \	Without Lime		
1	MP 16.77 WB	5255 54 7980	73,293	33,024	45
2	MP 16.77 WB	##	63,049	26,258	42
3	MP 16.77 WB		57,740	20,041	35
Averag	e		64,694	26,441	
b) With Lime					
4	MP 17.50 EB		159,096	90,521	57
5	MP 17.50 EB		149,816	86,154	58
6	MP 17.50 EB		158,125	91,942	58
Average	Э		155,679	89,539	58

Note: At the time of testing, the mix had 0.4% CMS-2S and 1.3% water.

Table 2. Summary of Test Results on Cores Obtained Eight Months after Construction

Sample	Lift		Resilient Mo	odulus (psi)		
I.D.	Location	(Top, in)	Unconditioned	F-T Conditioned	IRM (%)	
		a) \	Without Lime			
1	MP 16.75 WB	2.0	206,750	19,570	9	
2	MP 16.75 WB	2.3	235,420	27,420	12	
3	MP 16.75 WB	2.2	221,380	27,720	13	
Averag	е	221,183 24,903		11		
		b)	With Lime			
4	MP 17.50 EB	1.7	187,000	110,110	54	
5	MP 17.50 EB	1.9	180,350	110,520	61	
6	MP 17.50 EB	1.6	222,640	118,620	53	
Average	Э		196,663	113,083	56	

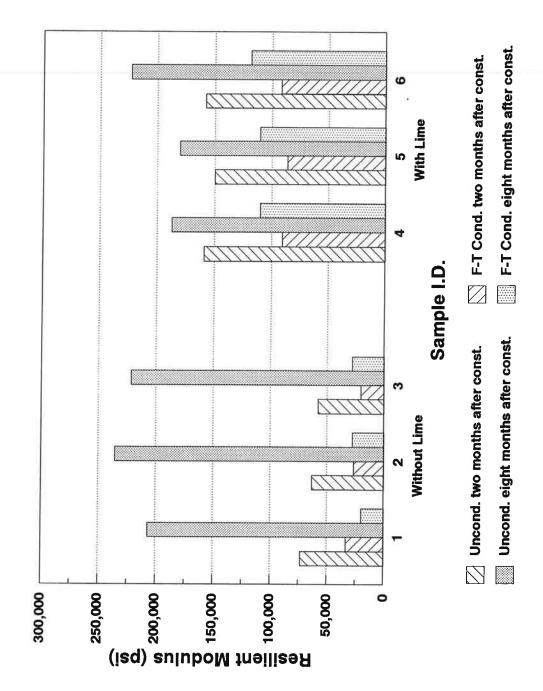


Figure 1 Resilient Modulus Test Results

3.5 <u>Discussion of Test Results</u>

Laboratory tests were conducted on recycled mix cores obtained two months after construction and the following is a discussion of the results. Laboratory test results on unconditioned core samples indicate that the resilient modulus of recycled mix with lime was approximately 140% greater than the resilient modulus of recycled mix without lime. Laboratory test results on freeze-thaw conditioned core samples indicated that the resilient modulus of the recycled mix with lime is also significantly higher than that of the recycled mix without lime. These characteristics may indicate that adding lime to the recycled mix may accelerate curing time and strength build-up.

Laboratory tests were also conducted on recycled mix cores obtained eight months after construction and the following is a discussion of the results. Laboratory test results on unconditioned core samples indicated that the resilient modulus for both mixes increased significantly with time, but the average resilient modulus value of the recycled mix with lime is similar to or slightly lower than that of the recycled mix without lime. This may indicate that the resilient modulus for both mixes would be the same after a period of time. However, laboratory test results on the freeze-thaw conditioned core samples indicated that the resilient modulus of the recycled mix with lime is significantly higher than that of the recycled mix without lime. This characteristic may indicate that adding lime to the recycled mix may improve its resistance to freeze-thaw damage.

4.0 CONCLUSIONS AND RECOMMENDATIONS

4.1 Conclusions

- For recycled mix core samples obtained two months after construction, the
 resilient modulus of the recycled mix with lime had a substantially higher resilient
 modulus compared to the recycled mix without lime. This may indicate that the
 added lime accelerated curing time and strength gain.
- 2. For recycled mix core samples obtained two and eight months after construction, the resilient modulus values of the recycled mix with lime after freeze-thaw conditioning were much higher than those of the recycled mix without lime. This may indicate that the recycled mix with lime have improved resistance to freeze-thaw damage compared to the recycled mix without lime.
- 3. For unconditioned recycled mix core samples obtained eight months after construction, the resilient moduli of both mixes are significantly higher than those two months after construction. However, eight months after construction, the average resilient modulus for each mix is similar. This may indicate the recycled mix with lime may not continue to increase its strength with time.

4.2 Recommendations

- Further evaluate the potential benefits of adding lime to the recycled mix and investigate the effects of adding different quantities of lime to the recycled mix.
- 2. Evaluate the effects of adding quick lime compared to hydrated lime to the recycled mix.
- 3. Appropriate mix design criteria, construction procedures, and field control guidelines should be developed if adding lime to the recycled mix.

APPENDIX A Correspondences

HIGHWAY DIVISION	RD	
1		LABORATORY NO.
		月10143
PROJECT	-10	DATA SHEET NO.
Arnold Ice caves - Horse	Ridge	A-30162
Central OR		EXP. ACCT. SUB JOB
CONTRACTOR	Deschute F.A. PROJECT NO.	M 009 - 4402 - 660 - 119 BID ITEM NO.
<u> </u>	Non	
PROJECT MANAGER	AGY.—ORG. UNIT	DATE RECEIVED DATE REPORTED
SUBMITTED BY	62 - 4000 AGYORG. UNIT	5-15-91 8-19-91
Source of MATERIAL		TEST NO. VAR LAB CHARGE
	02-4061 QUANTITY REPRESENTE	3-3158 \$ 249 00
SAMPLED AT SAMPLED BY		
SAME ELD BY	TO BE USED	DATE SAMPLED
MP 17.5 EB R. Sharte	ier Pavement	Evaluation 5-13-81
Core No. '	*1 *2	*3
Location MP	17.5 EB MP17.5	EB MP. 17.5 EB
	Top 1.7" Top	1.9" Top 1.6"
unconditioned Mr 1	87,000 180,3	
AVAIL NO.		
Index of Retained Mr		
That of Kelained / //	54% 61	2 53%
		RECEIVED AUG 1 9 1991 RESEARCH UNIT
DISTRIBUTION X Files X Project Manager REG 4 — RON SHARTNER Contractor Region Engineer X Region Assurance Specialist 4 Region Geologist Materials - Portland	specificationer For	this sample does, does not comply with information only.
Materials - Eugene	(2/10)

RESEARCH BIT MIX BILLQUINN

X X X 734-3069 (5-80)

Engineer of Material

TO:

Tony George

Boadway Materials Engineer

DATE:

November 8, 1990

FROM:

Dale D. Allen

NOTED Tony George

Region Engineer

Neil TO FYI

SUBJECT:

US 20

CIR Lime Study

This is to confirm our discussion on the scope of the above study and provide a little background data.

<u>Purpose of Study:</u> Does the addition of 2% lime improve the quality of CIR mixes and accelerate the strength development (curing). If the answer is positive to both questions, then we would consider greater use of lime in CIR projects in 1991.

Section Tested: This section of US 20 (MP 13.3-17.5) was an excellent old FLH project built in the mid-1970's (1975/76), Arnold Ice Caves-Horse Ridge Section. Rutting to one inch (3/4 average) and continuous fatigue cracking in all four wheel paths was the mode of failure.

<u>Lime Used:</u> 2% of quick lime was placed in EB lane for the entire 4 miles. $(MP\ 13.33-17.51)$

 ${\hbox{{\tt No Lime:}}\over\hbox{{\tt around}}}$ No lime was used when the single-unit recycle unit turned around (at Horse Ridge) and headed west. Therefore, the WB lane has no lime.

Recycle Agents Used:

EB (2% Lime) - MP 13.3-14.8 used 0.7 to 0.9% HFE 200 w/lime MP 14.8-16.8 used 0.6% HFE 200 w/lime

MP 15.8-17.5 used 0.4% CMS-2S w/lime

WB (No lime) - MP 14.1-15.5 used 0.2 to 0.3% CMS-2S

MP 15.5-16.73 used 0.4% CMS-2S

MP 17.5-17.4 used 0.5% CMS-2S

Core Location: To obtain similar sections, the cores with lime were cut in the EB lane at MP 17.51. (0.4% CMS-2S) The WB lane (w/o lime) had cores cut at MP 16.73 (0.4% CMS-2S). Three four-inch cores cut at both locations.

Observation of Cores: (November 8, 1990) - On this date, I observed the above 6 cores and the 3 cores cut in the lime section look excellent and did not break at the contact point. (At 2-inch depth) These will be sent to Salem today.

On the other hand, the cores broke when being cut in the sections w/o lime and after trimming would be less than $1\frac{1}{2}$ inches. I asked Ron Shartner to re-core and try to obtain 3 full-depth cores which you can trim to 2 inches.

The above observation clearly indicates some degree of improvement using lime. It appears the lime is accelerating the cure and strength gain.

Lab Samples: You should have lab samples requested by Dick Nelson this Spring, which provide the properties of the pavement before CIR. He sent in millings at MP 13, 14, 15, 16, 17, and 18.

DA:mr

Oregon

-August 20, 1991

Dr. David Rogge Construction-Engineering Project Mgmt. Dept. of Civil Engineering Oregon State University Corvallis, OR 97331 MUE CON DEPARTMENT OF

ASM RME CSS TRANSPORTATION

AA SME MRD

RUE FIS PET Highway Division

OSC AGG PHY Region 4

TSC BIT SOI

TTC CHE FISE FILE CODE:

RE: CIR Cores - US 20 Lab No's 10143-44

Attached are the Lab results of the cores on the cold recycle project in which one lane had lime and one lane did not.

I have requested the Materials and Research Section to provide an analysis.

It appears to me that the following conclusions can be drawn from this limited data.

Unconditioned M_R : The mixture, with and without lime, after 9 months has essentially the same modulus values, 190-200,000. This compares well with previous OSU Research.

Resistance to freeze-thaw: There is a significant and substantial improvement in the ability of the mixture with lime to resist freeze-thaw. MR without lime after freeze/thaw was only 20-27,000. MR with lime increased to 100-118,000. Likewise, this resulted in an increase Index of Retained MR from 10% to 55%.

Conclusion: It appears that the use of lime at a rate of $\pm 1.5\%$ can produce the following results.

- Accellerates the curing time and strength build-up. Field observations support this lab finding. Further research is needed to define the curing curve rate. In areas where CIR is performed in late fall or where the CIR will be covered with an overlay in two or three weeks after recycling, this use of lime would seem to be warranted.
- Lime does not appear to significantly change the strength after one year. Visual examination of cores, however, indicate that the CIR with lime appears to have fewer voids and is more dense. In the long term, you would expect this mixture to have better qualities.



P.O. Box 5309 Bend, OR 97708 FAX (503) 388-6231

R E . !AUG 2 2 1991 3. Lime significantly improves CIR to resist freeze-thaw damage. This is important for several reasons. First, we know that CIR without seals will crack in areas of frequent freeze-thaw. If lime is used, it allows (if necessary) to carry a CIR job through the first winter with a sand seal. The fact that the Highway 20 CIR has not shown freeze-thaw damage seems to support the laboratory results.

I have requested Bill Quinn to follow up with additional research on the I-84 CIR project.

A question I have is whether we could not get equal or better results by introducing the lime as a slurry in front of the mill. This would seem to provide more uniform mixing and control. Also, would slacked vs. quick lime work equally as well without the steam problem? How much lime to use? Very limited data indicates that about $1\frac{1}{2}\%$ is optimum, but we should do some research on 1%, 1.5%, 2%.

Bill Quinn advised he would meet with Region 4 and develop strategy for additional research.

Dale D. Allen, P.E.

Region Engineer

DA:mr

encl

cc: Gary Hicks
Bill Quinn
Dick Nelson

APPENDIX B Laboratory Test Results

	ORATORY	RECORD	LABORATORY	NO.			
HIGHWAY DIVISION				9013575			
PROJECT			DATA SHEET N	10.			
ARNOLD ICE CAVE - HO	RSE RIDGE	78511057		A-30155			
. Central Oregon		Descutes		4402 000 119			
CONTRACTOR		FA PROJECT NO.	1100)	BID ITEM NO.			
ROJECT MANAGER		AGY, - ORG, UNIT	None DATE RECEIVED	DATO-DEDOCTED			
Dale Allen		02-4000	11-30-90 TEST NO.	DATE DECRES 4 1990			
RonShartner OURCE OF MATERIAL		AGYORG.UNIT 02-4061 3x	302 D	VAR. LAB CHARGE			
M.P. 16.77 WB 9'			3150	\$324°°			
MP 16.77 WB 9' R Shar		TOBEUSED Pavement Evalu	ation	11-29-90			
Core #	1	2	3				
Location	MP 16.77	MP 16.77	MP 16.77	***			
Lift	top	top	top				
Unconditioned Mr	73,293	63,049	57,740				
Freeze - Thaw conditioned Mr	33,024	26,258	20,041				
Index of Retained Mr	45.1	41.6	34.7				
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JMBER	ACCEPTED	DATE	G 8	REJECTED			

REMARKS

734-3069 (3-90)

Oregon Department of Transportation HIGHWAY DIVISION	.ABORATOR	Y RECORD	Page LABORATORY NO.				
عاد				9013344			
ARNOLD ICE CAVE - HO	RSE RIDGE		DATA SHEET NO.	A-30154			
Gon hara 1 Constant		COUNTY					
Central Oregon		Deschut	es M00944	02-000-119			
		FA PROJECT NO. None		BID ITEM NO.			
ROJECT MANAGER Dale Allen		AGY ORG. UNIT 02-4000	DATE RECEIVED	DATE BEPARTED 4 1990			
Ron Shartner		AGYORG. UNIT 02-4061 32	TEST NO. V.	AR. LAB CHARGE			
OURCE OF MATERIAL M.P. 17.5 EB	4.5'	QUANTITY REPRESENTED					
AMPLED AT SAMI	PLED BY	TO BE USED	(3150)	\$324 SE DATE SAMPLED 10-31-90			
M.P. 17.5 EB 4.5' R	Shartner	Pavement Eval	uation	10-31-90			
Core	# 1	2	3				
Location	n MP 17.5 E	B MP 17.5 EB	MP 17.5 EB				
Lift	top	top	top				
Unconditioned l	M _r 159,096	149,816	158,125				
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SAMPLE NO. HT/LOT NO. /ROLL NO. SPEC. NO. MARK OTHER (EXPLAIN BELOW)

TAYA-3069 (3-90)

Oregon Department of Transportation LABC	RATORY RE	CORD						
HIGHWAY DIVISION	- ·	· - _				LABORATORY NO.		44
Arnold ice Caves	- 140,550	w is			-	DATA SHEET NO. A - 30	- · ·	7
HIGHWAY	110V 3-C	wiage	COUN	ITY	_	EXP. ACCT. SUB JO		<u>5</u>
Centra OR.				eschutes		M 609 -4		-000-18
ROTSARTINOS			F.A. P	ROJECT NO.		1.00		DITEM NO.
PROJECT MANAGER				None	2			
Pale Allen				-ORG. UNIT		DATE RECEIVED		TE REPORTED
SUBMITTED BY			02	2-4000 ORG. UNIT		5-15-91		3-14-9
Ron Shartner Source OF MATERIAL			DOS DAYS	2-4061				B CHARGE
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